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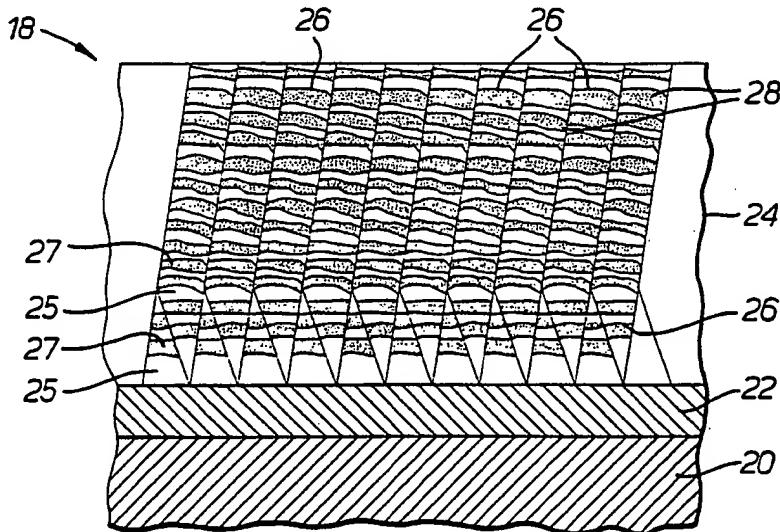
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(57) Abstract

A superalloy turbine blade (10) has a MCrAlY bond coating (22) and a thermal barrier coating (24). The thermal barrier coating (24) comprises a plurality of alternate layers (25, 27) which have different structure to produce a plurality of interfaces (26) substantially parallel to the metallic substrate (20)/bond coating (22) interface. These interfaces (26) provide paths of increased resistance to heat transfer to reduce the thermal conductivity of the thermal barrier coating (24). The structure in the alternate layers (25, 27) of the thermal barrier coating (24) is columnar (28), or segmented, to ensure that the strain tolerance of the thermal barrier coating (24) is not impaired. The columnar grains (28) in the layers (25, 27) extend substantially perpendicular to the metallic substrate (20)/bond coating (22) interface. This enables thermal barrier coatings (24) of reduced thickness and weight to be used. The bond coating may have an oxide or oxide/metal interface which improves the adhesion of the thermal barrier coating.

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A COATED ARTICLE

The present invention is concerned with coatings for metallic substrates, and is particularly concerned with ceramic thermal barrier coatings for metallic components for use in gas turbine engines.

5 It is known in the prior art to apply ceramic to a metallic substrate to produce a ceramic thermal barrier coating by the thermal, or plasma, spray process. In this technique the ceramic is applied onto a bond coat, for example a MCrAlY bond coat, which has been applied to the 10 metallic substrate.

It is also known in the prior art to apply ceramic to a metallic substrate to produce a ceramic thermal barrier coating by the physical vapour deposition (PVD) process. In this technique the ceramic is applied onto a 15 bond coat, for example a MCrAlY coating with an alumina interface layer, which has been applied to the metallic substrate. The ceramic thermal barrier coatings deposited by the PVD process have benefits over the ceramic thermal barrier coatings deposited by a thermal spray process.

20 The main benefit is improved thermal shock resistance due to the columnar structure of the ceramic thermal barrier coating produced by the PVD process. Other benefits are improved erosion resistance and improved aerothermal performance.

25 However, despite these advantages, the ceramic thermal barrier coating deposited by the PVD process exhibits a thermal conductivity which is greater than that of a ceramic thermal barrier coating, of the same or similar composition, deposited by the thermal spray process. For example the thermal conductivity of a zirconia-8% yttria ceramic thermal barrier coating deposited by the PVD process is 2.0 W/m/K and the thermal conductivity for the same ceramic thermal barrier coating deposited by the thermal spray process is 0.8-1.0 W/m/K.

30 35 If all other factors are the same for the two methods of deposition of the ceramic thermal barrier coating, the

greater thermal conductivity of the ceramic thermal barrier coating deposited by the PVD process means that a greater thickness of ceramic is required to achieve the equivalent insulating effect when compared to the ceramic thermal barrier coating deposited by the thermal spray process. This is an undesirable property because this necessitates a greater weight of ceramic thermal barrier coating on the metallic components of the gas turbine engine, and this is particularly undesirable for rotating components e.g. turbine blades because the additional weight may limit the temperature of operation due to a corresponding reduction in the creep life of the metallic turbine blade.

A paper entitled "Microlaminate Composites as Thermal Barrier Coatings" by M.C.Radhakrishna, H.J. Doerr, C.V. Deshpandey and R.F. Bunshah was presented at the 15th International Conference on Metallurgical Coatings, at San Diego, USA, 11-15th April 1988 and was subsequently presented in Surface and Coatings Technology, 36 (1988) 143-150. The paper discloses the use of microlaminate composites to reduce the thermal conductivity of physical vapour deposited thermal barrier coatings. The microlaminate composites comprise alternate layers of two different materials, e.g. two different metals, two different ceramics or a metal and a ceramic. The paper specifically describes the use of nickel layers interposed between layers of NiCoCrAlY and titanium layers interposed between layers of CoCrAlY. These microlaminates have thermal conductivities of 7.48 W/m/K for a 480 layer Ni/NiCoCrAlY coating system and 6.76 W/m/K for a 480 layer Ti/CoCrAlY coating system. The paper then suggests that the thermal conductivity of the microlaminate composite may be tailored to obtain thermal conductivity values similar to those of yttrium stabilised zirconia deposited by the thermal spray process by choosing appropriate metal and ceramic microlaminates.

A paper entitled "Sputter-Deposited Multilayered Ceramic/Metal Coatings" by J.W. Patten, M.A. Bayne, D.D. Hayes, R.W. Moss and E.D. McClanahan was presented at the International Conference on Metallurgical Coatings, San 5 Diego, USA, 23-27th April 1979 and was subsequently presented in Thin Solid Films, 64 (1979) 337-343. The paper discloses the use of alternate layers of metal and ceramic. The ceramic layers are to provide erosion, corrosion and possibly thermal insulation, while the 10 metal layers improve mechanical properties. The metal and ceramic layers are sputter deposited. The alternate layers described were nickel interposed between yttria stabilised zirconia and nickel-chromium interposed between yttria stabilised zirconia. The ceramic layers 15 are of the columnar type.

A further disclosure in published European patent application 0366289A entitled "Multi-Layer Wear Resistant Coatings" uses alternate layers of metallic and ceramic materials to provide an erosion and corrosion resistant 20 coating. This discloses layers of titanium and titanium nitride but metal layers of boron, zirconium, hafnium, tantalum or iron may be used and ceramic layers of a nitride, a carbide or an oxide of these metals may be used. The coatings may be applied by sputtering, physical 25 vapour deposition or chemical vapour deposition.

We believe that the concept of inserting metallic layers between layers of ceramic to provide improved performance with regard to the thermal conduction, i.e. to reduce the thermal conductivity and coating ductility 30 of a thermal barrier coating is unsound for the following reasons. It is not thought likely that such an approach will lead to a reduction in the thermal conductivity of the thermal barrier coating and the metal layers will become oxidised leading to instability of the thermal 35 barrier coating.

Furthermore, the use of layers of different materials in a thermal barrier coating necessitates the

use of separate sources of metal and ceramic which have to be evaporated, or sputtered, to deposit the alternate layers on the metallic substrate. Alternatively reactive gas sources have to be available to provide reactive gas 5 to react with the evaporated metal to produce the ceramic layers.

A paper entitled "Ceramic Thermal Barrier Coatings with Improved Corrosion Resistance" by J.T. Prater and E.L. Courtright was presented at the 14th International 10 Conference on Metallurgical Coatings, San Diego, USA, 23-27th March 1987 and was subsequently presented in Surface and Coatings Technology, 32 (1987) 389-397. The paper discloses a method for limiting the ingress of corrosive species in physical vapour deposited yttria 15 stabilised zirconia ceramic thermal barrier coatings by inserting dense ceramic sealing layers between the usual columnar ceramic layers. The dense ceramic sealing layers disrupt the columnar ceramic layers to reduce the permeability to liquid and gaseous species and increases 20 the corrosion resistance of the ceramic thermal barrier coating.

The columnar layers were deposited by sputtering and the dense ceramic sealing layers were deposited by sputtering and applying a RF induced DC bias on the 25 substrate. The voltage applied during the period that the bias is applied to the substrate causes renucleation/grain growth within the coating structure and destroys the major, through thickness, columnar boundaries between columnar grains.

30 However, this paper does not disclose any details of the effect of the dense ceramic sealing layers on the thermal conductivity of the ceramic thermal barrier coating.

The present invention seeks to provide an article 35 which comprises a metallic substrate having a columnar thermal barrier coating in which the thermal barrier coating has reduced thermal conductivity.

Accordingly the present invention provides an article comprising a metallic substrate, a bond coating on the metallic substrate, a thermal barrier coating on the bond coating, the thermal barrier coating comprising 5 a plurality of layers, each layer having columnar grains, the columnar grains in each layer extending substantially perpendicular to the interface between the bond coating and the metallic substrate, adjacent layers having different structures to provide at least one interface 10 between adjacent layers which is substantially parallel to the interface between the bond coating and the metallic substrate to increase the resistance to heat transfer through the thermal barrier coating.

The metallic substrate may be a superalloy 15 substrate. The superalloy substrate may be a nickel superalloy substrate.

The bond coating may comprise a MCrAlY coating, an aluminide coating, platinum aluminide coating or a combination of any two or more thereof. For example a 20 MCrAlY coating may be provided with an aluminide coating to provide more aluminium content to bond the thermal barrier coating onto the substrate. The bond coating may include an interface layer comprising an oxide or oxide/metal, the thermal barrier coating being on the 25 interface layer.

The thermal barrier coating may be formed from a ceramic material. The ceramic material may comprise zirconia, yttria or a mixture thereof.

Alternate layers of the thermal barrier coating may 30 have substantially the same structure.

Adjacent layers may have substantially the same thickness. The thickness of each layer may be in the range of 0.5×10^{-6} m to 10×10^{-6} m. Preferably the thickness of each layer is 2×10^{-6} m. The total thickness 35 of the thermal barrier coating may be up to 300×10^{-6} m.

The layer adjacent to the bond coating may have a high density, preferably the layer adjacent the bond

coating has maximum density.

The article may be a turbine blade or turbine vane.

The present invention also seeks to provide a method of manufacturing an article comprising applying a bond 5 coating to a metallic substrate, applying a thermal barrier coating to the bond coating by depositing at least one columnar grained layer by vapour deposition and depositing at least one columnar grained layer by plasma assisted vapour deposition to provide an interface 10 between the adjacent layers which is substantially parallel to the interface between the bond coating and the metallic substrate to increase the resistance to heat transfer through the thermal barrier coating.

Preferably depositing the columnar grained layers 15 deposited by vapour deposition alternately with the columnar grained layers deposited by plasma assisted vapour deposition.

Preferably depositing the columnar grained layer adjacent the bond coating by plasma assisted vapour 20 deposition such that it has a high density, preferably depositing the columnar grained layer adjacent to the bond coating such that it has maximum density.

Preferably applying an electrical bias to the metallic substrate and supplying oxygen to modify the 25 bond coating surface to produce an interface layer comprising oxide or oxide/metal prior to deposition of the columnar grained layers by vapour deposition process.

Preferably applying an electrical bias to the metallic substrate and supplying an inert gas to produce 30 ions to clean the surface of the bond coating prior to the formation of the interface layer.

Preferably depositing the columnar grained layers deposited by vapour deposition and the columnar grained 35 layers deposited by plasma assisted vapour deposition such that they have substantially the same thickness.

Preferably the vapour deposition process is physical vapour deposition. The physical vapour deposition process

may be electron beam evaporation, sputtering or arc evaporation.

5 Depositing the columnar grained layers to a thickness of 0.5×10^{-6} m to 10×10^{-6} m. Depositing the columnar grained layers to a total thickness up to 300×10^{-6} m.

10 Preferably applying the bond coating by thermal spraying, the bond coating may comprise MCrAlY coating, an aluminide coating, platinum aluminide coating or a combination of any two or more thereof.

The metallic substrate may be a superalloy substrate. The thermal barrier coating may comprise a ceramic material. The ceramic material may be zirconia or yttria or a mixture thereof.

15 The present invention also provides an article comprising a metallic substrate, a bond coating on the metallic substrate, a thermal barrier coating on the bond coating, the thermal barrier coating having columnar grains, the columnar grains extending substantially perpendicular to an interface between the bond coating and the metallic substrate, each of the columnar grains in the thermal barrier coating comprising a plurality of layers, adjacent layers having different structures to provide at least one interface between adjacent layers 20 which is substantially parallel to the interface between the bond coating and the metallic substrate to increase 25 the resistance to heat transfer through the thermal barrier coating.

The present invention will be more fully described 30 by way of example, with reference to the accompanying drawings in which:-

Figure 1 is a perspective view of a gas turbine engine turbine blade according to the present invention.

35 Figure 2 is a sectional view through an article having a thermal barrier coating applied by a first prior art method.

Figure 3 is a sectional view through an article

having a thermal barrier coating applied by a second prior art method.

Figure 4 is a sectional view through an article having a thermal barrier coating applied according to the 5 present invention.

Figure 5 is an enlarged view of a portion of the thermal barrier coating shown in figure 4.

Figure 6 is a graph of voltage applied to the substrate against time during the application of the 10 thermal barrier coating.

Figure 7 is a sectional view through an apparatus for use in the method of applying the thermal barrier coating according to the present invention.

Figure 8 is a graph of thermal conductivity against 15 temperature for several thermal barrier coatings.

Figure 9 is a sectional view through an article having an alternative thermal barrier coating applied according to the present invention.

Figure 10 is an enlarged view of a portion of the 20 thermal barrier coating in Figure 9.

Figure 11 is a graph of voltage applied to the substrate against time during the application of the thermal barrier coating.

Figure 12 is a graph of current density against 25 substrate voltage.

Figure 13 is a graph of current density against pressure.

Figure 14 is a micrograph of a fracture cross-section through an article according to the present 30 invention.

A gas turbine engine turbine blade 10 is shown in figure 1. The turbine blade 10 comprises a shaped root portion 12, for attaching the turbine blade 10 to a turbine rotor, a platform portion 14, for defining a 35 portion of the radially inner boundary of the gas flow path through the turbine, and an aerofoil portion 16, which extracts energy from the hot gases passing through

the turbine. The platform portion 14, and the aerofoil portion 16, of the turbine blade 10 are provided with a coating system 18 which allows the turbine blade 10 to operate at higher gas temperatures.

5 The coating system 18 comprises a bond coating 22, deposited onto the metallic substrate 20 of the turbine blade 10, and a ceramic thermal barrier coating 24 deposited onto the bond coating 22.

A coating system 38 applied by a first prior art 10 method is shown in figure 2. The coating system 38 comprises a bond coating 42, deposited onto the metallic substrate 40 and a ceramic thermal barrier coating 44 deposited onto the bond coating 42. The bond coating 42 is generally a MCrAlY coating which has been deposited by 15 thermal spraying or by physical vapour deposition (PVD), or the bond coating may be an aluminide coating. The bond coating 42 may additionally have an alumina layer. The ceramic thermal barrier coating 44 is generally zirconia or yttria or a mixture thereof which has been deposited 20 onto the bond coating 42 by physical vapour deposition (PVD). The ceramic thermal barrier coating 44 has a columnar grained microstructure 46 which has a relatively high thermal conductivity, good strain tolerance, good surface finish and good erosion resistance.

25 A coating system 48 applied by a second prior art method is shown in figure 3. The coating system 48 comprises a bond coating 52, deposited onto the metallic substrate 50 and a ceramic thermal barrier coating 54 deposited onto the bond coating 52. The bond coating 52 is generally a MCrAlY coating which has been deposited by 30 thermal spraying or by physical vapour deposition (PVD), or the bond coating may be an aluminide coating. The ceramic thermal barrier coating 54 is generally zirconia or yttria or a mixture thereof which has been deposited 35 onto the bond coating 52 by thermal spraying. The ceramic thermal barrier coating 54 has a "brick wall" microstructure which has poor erosion resistance but has

a relatively low thermal conductivity when compared to the thermal conductivity of the ceramic thermal barrier coating applied by the first prior art method mentioned above.

5 The coating system 18 applied by the method of the present invention is shown more clearly in figures 4 and 5. The coating system 18 comprises a bond coating 22, deposited onto the metallic substrate 20 and a ceramic thermal barrier coating 24 deposited onto the bond 10 coating 22.

The bond coating 22 is generally a MCrAlY coating which has been deposited by thermal spraying or by physical vapour deposition (PVD). Alternatively the bond coating 22 may be an aluminide coating which has been 15 deposited by pack aluminising or may be a platinum-aluminide coating which has been deposited by platinum aluminising.

The ceramic thermal barrier coating 24 is generally zirconia, yttria or a mixture thereof which has been 20 deposited onto the bond coating 22 by physical vapour deposition (PVD). Alternatively the ceramic thermal barrier coating 24 may comprise any other suitable ceramic. The ceramic thermal barrier coating 24 has a columnar grained microstructure 28 which has good strain 25 tolerance, good surface finish and good erosion resistance. The ceramic thermal barrier coating 24 has a relatively low thermal conductivity when compared to the ceramic thermal barrier coating 44 of the coating system 38 in figure 2 and is substantially the same or better 30 than the thermal conductivity of the ceramic thermal barrier coating 54 of the coating system 48 in figure 2. The ceramic thermal barrier coating 24 in figures 4 and 5 has reduced thickness compared to the ceramic thermal barrier coating 44 in figure 2 for operation at the same 35 temperature. Alternatively the same thickness of ceramic thermal barrier coating 24 may be used to allow operation at higher temperatures.

The ceramic thermal barrier coating 24 has alternate layers 25 and 27 which have different structure to create interfaces 26 substantially parallel to the metallic substrate 20/bond coating 22 interface. These interfaces 5 26 provide paths of increased resistance to heat transfer to emulate the good thermal conductivity properties of thermal sprayed ceramic thermal barrier coatings. The structure in the alternate layers 25,27 of the ceramic thermal barrier coating 24 is columnar 28 to ensure that 10 the strain tolerance of the ceramic thermal barrier coating 24 is not impaired. The columnar grains 28 in the layers 25,27 extend substantially perpendicular to the metallic substrate 20/bond coating 22 interface. The difference in structure in layers 25, 27 are the result 15 of variations in the micro-structure and/or density/coarseness of the columnar grains 28 of the ceramic.

It is to be noted that the columnar grains 28 in one of the layers 27 continue to grow into the adjacent layer 20 25 and that there is no interruption of the columnar grains 28 at the interfaces 26 between the layers 25,27. It may also be considered that the columnar grains 28 in the ceramic thermal barrier coating 24 extend through the full thickness of the coating 24, and that each columnar 25 grain 28 has its structure modulated along its length by the provision of the layers 25,27.

The coating system 18 according to the present invention is applied to the metallic substrate 20 by firstly depositing a MCrAlY bond coating 22 onto the 30 metallic substrate 20 by plasma spraying. Alternatively the MCrAlY may be deposited by physical vapour deposition (PVD). A ceramic thermal barrier coating 24 is then deposited onto the MCrAlY bond coating 22.

An apparatus used for depositing the ceramic thermal 35 barrier coating 24 onto the MCrAlY bond coating 22 is shown in figure 7. The apparatus 60 comprises a vacuum chamber 62 which has one or more pumps 64 to evacuate the

vacuum chamber 62. An electron beam from an electron beam gun 66 is arranged to impinge upon a supply of ceramic vapour 68, i.e zirconia-ytria alloy, such that the ceramic is evaporated when the vacuum chamber 62 is 5 evacuated. The metallic substrate 20 is also connected into an electrical circuit such that it may given a D.C. or R.F. potential 70. The apparatus 60 also includes supplies of argon 74, hydrogen 76 and oxygen 78 which are interconnected to the interior of the vacuum chamber 62 10 via a pipe 72. Each of the supplies of argon 74, hydrogen 76 and oxygen 78 are provided with valves to control the flow of the gases.

In order to deposit the ceramic thermal barrier coating 24 onto the MCrAlY bond coating 22 the metallic substrate 20 with the deposited bond coating 22 is placed 15 into the vacuum chamber 62. The vacuum chamber 62 is evacuated and the electron beam gun 66 directs electrons at the supply of ceramic vapour 68 to evaporate ceramic. The interior of the vacuum chamber 62 is supplied with 20 controlled amounts of an inert gas and oxygen during the evaporation of the supply of ceramic vapour 68. The supply of inert gas, e.g. argon, is to maintain the correct glow discharge, or plasma, conditions and the supply of oxygen is to maintain the composition of the 25 ceramic thermal barrier coating at the stoichiometric ratio. The ceramic vapour deposits onto the MCrAlY bond coating 22. In order to produce the layers 25 and 27 in the ceramic thermal barrier coating 24, the ceramic vapour is deposited alternately, for predetermined 30 periods of time, by the physical vapour deposition process (PVD) and by a plasma assisted physical vapour deposition process (PAPVD). In the plasma assisted physical vapour deposition process (PAPVD) a D.C. or R.F. potential is applied to the metallic substrate 20, this 35 is known as ion plating.

The first layer 25 of ceramic deposited onto the bond coating 22 is preferably deposited by plasma

assisted physical vapour deposition (PAPVD) such that the ceramic at the interface with the bond coating 22 has a relatively high density and preferably has maximum density.

5 The use of the plasma assisted physical vapour deposition process (PAPVD) is used to control the structure of the ceramic thermal barrier coating 24 all the way through its thickness, by controlling the way that the columnar ceramic grains 28 grow, to tailor the
10 characteristics of the ceramic at particular positions. The plasma assisted physical vapour deposition process (PAPVD) causes the columnar ceramic grains 28 to be packed together more closely. The D.C. or R.F. potential used during the plasma assisted physical vapour
15 deposition process (PAPVD) may be adjusted for deposition of different ceramic layers to control the density of the columnar ceramic grains 28.

20 In order to achieve the maximum difference in thermal conductivity between adjacent layers 25,27, the interfaces 26 between the adjacent layers 25,27 should be as abrupt as is practical. The abrupt interfaces 26 are preferably achieved by the use of a simple switching action between the physical vapour deposition process and the plasma assisted physical vapour deposition process
25 such that the voltage at the substrate follows a square wave form with time as shown in figure 6. The peak voltages in figure 6 correspond to the time when the layers 25 of ceramic are deposited by plasma assisted physical vapour deposition and the minimum voltages in
30 figure 6 correspond to the time when the layers 27 of ceramic are deposited by physical vapour deposition. The switching points in figure 6 correspond to the time when the interfaces 26 between the layers 25 and 27 are produced.

35 In an experiment four different coating systems were applied to a metallic substrate. The first coating system comprised a plasma sprayed MCrAlY bond coating applied

onto a nickel superalloy, N75 a nickel-chromium superalloy, and a purely physical vapour deposited (PVD) ceramic thermal barrier coating applied onto the bond coating. The vacuum chamber was evacuated to a pressure of 5 mTorr and the electron beam gun power was 8KV at 500mA. A total coating thickness of 90×10^{-6} m was deposited. The thermal conductivity of the ceramic thermal barrier coating was measured at a temperature of 1000°C and was 1.0 W/m/K.

10 The second coating system comprised a plasma sprayed MCrAlY bond coating applied onto the same nickel superalloy and a purely plasma assisted physical vapour deposited (PAPVD) ceramic thermal barrier coating applied onto the bond coating. The vacuum chamber was evacuated 15 to a pressure of 7 mTorr and the electron beam gun power was 8KV at 500mA. The R.F. power used during the PAPVD process was 500W. A total ceramic coating thickness of 160×10^{-6} m was deposited. The thermal conductivity of the ceramic thermal barrier coating was measured at a 20 temperature of 1000°C and was 0.55 W/m/K.

The third coating system comprised a plasma sprayed MCrAlY bond coating applied onto the same nickel superalloy and alternate layers of physical vapour deposited (PVD) and plasma assisted physical vapour 25 deposited (PAPVD) ceramic thermal barrier coating applied onto the bond coating. The vacuum chamber was evacuated to a pressure of 4 mTorr and the electron beam gun power was 8KV at 500mA. The R.F. power used during the PAPVD process was 500W. A total of 70 layers of ceramic were 30 deposited. Each of the 35 layers of ceramic deposited by the physical vapour deposition process (PVD) were 2×10^{-6} m thick and each of the 35 layers of ceramic deposited by the plasma assisted physical vapour 35 deposition process (PAPVD) were also 2×10^{-6} m thick. The thermal conductivity of the ceramic thermal barrier coating was measured at a temperature of 1000°C and was 0.3 W/m/K.

The fourth coating system comprised a plasma sprayed MCrAlY bond coating applied onto the same nickel superalloy and alternate layers of physical vapour deposited (PVD) and plasma assisted physical vapour deposited (PAPVD) ceramic thermal barrier coating applied onto the bond coating. The vacuum chamber was evacuated to a pressure of 4 mTorr and the electron beam gun power was 8KV at 500mA. The R.F. power used during the PAPVD process was 500 W. A total of 70 layers of ceramic were deposited. Each of the 35 layers of ceramic deposited by the physical vapour deposition process (PVD) were 2×10^{-6} m thick and each of the 35 layers of ceramic deposited by the plasma assisted physical vapour deposition process (PAPVD) were 1×10^{-6} m thick. The thermal conductivity of the ceramic thermal barrier coating was measured at a temperature of 1000°C and was 1.0 W/m/K.

Figure 8 shows a graph of thermal conductivity against temperature for each of the four different coating systems. Line A indicates the thermal conductivity of the first coating system with temperature. Line B indicates the thermal conductivity of the second coating system with temperature. Line C indicates the thermal conductivity of the third coating system with temperature and finally line D indicates the thermal conductivity of the fourth coating system with temperature.

The thermal conductivity of the third coating system is a third of that of the first coating system. The first coating system is the ceramic thermal barrier coating applied by the prior art method of physical vapour deposition (PVD). The thermal conductivity of the third coating system is also less than that of the second coating system. The second coating system is the ceramic thermal barrier coating applied purely by plasma assisted physical vapour deposition (PAPVD).

The thermal conductivity of the fourth coating

system is approximately the same as the first coating system.

5 A further coating system 88 applied by the method of the present invention is shown more clearly in figures 9 and 10. The coating system 88 comprises a bond coating 92, deposited onto the metallic substrate 90, an interface layer 94 on the bond coating 92 and a ceramic thermal barrier coating 96 deposited onto the interface layer 94.

10 The bond coating 92 is generally a MCrAlY coating which has been deposited by thermal spraying or by physical vapour deposition (PVD). Alternatively the bond coating 92 may be an aluminide coating which has been deposited by pack aluminising or may be a 15 platinum-aluminide coating which has been deposited by platinum aluminising. The bond coating 92 may be a MCrAlY coating with an aluminide top coating or a MCrAlY coating with a platinum aluminide top coating.

The interface layer 94 comprises oxides or 20 oxide/metal on the bond coating which improves the adhesion of the ceramic thermal barrier coating 96. The oxide is predominantly alumina which has controlled structure and properties. The metal comprises the metallic elements in the bond coating.

25 The ceramic thermal barrier coating 96 is generally zirconia, yttria or a mixture thereof which has been deposited onto the interface layer 94 by physical vapour deposition (PVD). Alternatively the ceramic thermal barrier coating 96 may comprise any other suitable 30 ceramic. The ceramic thermal barrier coating 96 has a columnar grained microstructure 100 which has good strain tolerance, good surface finish and good erosion resistance. The ceramic thermal barrier coating 96 has a relatively low thermal conductivity when compared to the 35 ceramic thermal barrier coating 44 of the coating system 38 in figure 2 and is substantially the same or better than the thermal conductivity of the ceramic thermal

barrier coating 54 of the coating system 48 in figure 3. The ceramic thermal barrier coating 96 in figures 9 and 10 has reduced thickness compared to the ceramic thermal barrier coating 44 in figure 2 for operation at the same 5 temperature. Alternatively the same thickness of ceramic thermal barrier coating 96 may be used to allow operation at higher temperatures.

The ceramic thermal barrier coating 96 has alternate layers 97 and 98 which have different structure to create 10 interfaces 99 substantially parallel to the metallic substrate 90/bond coating 92 interface. These interfaces 99 provide paths of increased resistance to heat transfer to emulate the good thermal conductivity properties of thermal sprayed ceramic thermal barrier coatings. The 15 structure in the alternate layers 97,98 of the ceramic thermal barrier coating 96 is columnar 100 to ensure that the strain tolerance of the ceramic thermal barrier coating 96 is not impaired. The columnar grains 100 in the layers 97,98 extend substantially perpendicular to 20 the metallic substrate 90/bond coating 92 interface. The difference in structure in layers 97, 98 are the result of variations in the structure and/or density/coarseness of the columnar grains 100 of the ceramic.

The columnar grains 100 in one of the layers 98 25 continue to grow into the adjacent layer 97 and there are no interruptions of the columnar grains 100 at the interfaces 99 between the layers 97,98. The columnar grains 100 in the ceramic thermal barrier coating 96 extend through the full thickness of the coating 96 and 30 each columnar grain 100 has its structure modulated along its length by the provision of the layers 97,98.

The coating system 88 according to the present invention is applied to the metallic substrate 90 by firstly depositing a MCrAlY bond coating 92 onto the 35 metallic substrate 90 by plasma spraying. Alternatively the MCrAlY may be deposited by physical vapour deposition

(PVD). The surface of the bond coating 92 is then modified to create an oxide or oxide/metal interface layer 94 which has controlled structure and properties to improve the adhesion of the subsequently deposited 5 ceramic thermal barrier coating 96. A ceramic thermal barrier coating 96 is then deposited onto the interface layer 94.

In order to create the interface layer 94 on the surface of the bond coating 92 and to deposit the ceramic 10 thermal barrier coating 96 onto the interface layer 94 the metallic substrate 90 with the deposited bond coating 92 is placed into the vacuum chamber 62.

The vacuum chamber 62 is evacuated and an electrical bias, e.g. a D.C. potential or R.F. field, is applied to 15 the metallic substrate 90 prior to the deposition of the columnar grained ceramic thermal barrier coating 96 in order to modify the structure and/or chemistry of the surface of the bond coating 92. Controlled amounts of gases are introduced into the interior of the vacuum 20 chamber 62 during this phase of the process, for example argon-oxygen, argon-hydrogen or argon. The electrical bias produces chemically active glow discharges or plasmas in the case of argon-oxygen and argon-hydrogen, or produces neutral glow discharges or plasmas in the 25 case of argon. The argon plasma may be used to produce argon ions which bombard the surface of the bond coating 92 to clean the surface i.e. to remove undesired oxides and/or any contaminants. The argon-hydrogen plasma may be used to provide enhanced cleaning of the surface of the 30 bond coating 92 because the additional hydrogen ions chemically react with the undesired contaminants. When the surface of the bond coating 92 is cleaned of undesired oxides and/or contaminants the argon-oxygen plasma, or argon-hydrogen plasma, provides controlled 35 production of desired bonding oxides in an interface 94 on the surface of the bond coating 92. The interface 94 improves the adhesion of the subsequently deposited

ceramic thermal barrier coating 96. The gases used during the modification of the surface of the bond coating 92 to produce the interface layer 94 are then extracted from the vacuum chamber 62.

5 The electron beam gun 66 directs electrons at the supply of ceramic vapour 68 to evaporate ceramic. The interior of the vacuum chamber 62 is supplied with controlled amounts of an inert gas and oxygen during the evaporation of the supply of ceramic vapour 68. The 10 supply of inert gas, e.g. argon, is to maintain the correct glow discharge, or plasma, conditions and the supply of oxygen is to maintain the composition of the ceramic thermal barrier coating at the stoichiometric ratio. The ceramic vapour deposits onto the interface 15 layer 94. In order to produce the layers 97 and 98 in the ceramic thermal barrier coating 96, the ceramic vapour is deposited alternately, for predetermined periods of time, by the physical vapour deposition process (PVD) and by a plasma assisted physical vapour deposition process 20 (PAPVD). In the plasma assisted physical vapour deposition process (PAPVD) a D.C. or R.F. potential is applied to the metallic substrate 90.

The first layer 97 of ceramic deposited onto the interface layer 94 is preferably deposited by plasma 25 assisted physical vapour deposition (PAPVD) such that the ceramic at the interface with the interface layer 94 has a relatively high density and preferably has maximum density.

30 The use of the plasma assisted physical vapour deposition process (PAPVD) is used to control the structure of the ceramic thermal barrier coating 96 all the way through its thickness, by controlling the way that the columnar ceramic grains 100 grow, to tailor the characteristics of the ceramic at particular positions. 35 The plasma assisted physical vapour deposition process (PAPVD) causes the columnar ceramic grains 100 to be packed together more closely. The D.C. or R.F. potential

used during the plasma assisted physical vapour deposition process (PAPVD) may be adjusted for deposition of different ceramic layers to control the density of the columnar ceramic grains 100.

5 In region A of figure 11 an initial large voltage is applied to the metallic substrate 90 to modify the structure and/or chemistry of the surface of the bond coating 92. The magnitude of the initial large voltage is determined by the need to remove contaminants or
10 undesirable oxides from the bond coating 92 prior to establishing the desired oxide structure-composition to achieve satisfactory adhesion of the thermal barrier coating 96. The desired oxide may be grown thermally or in the presence of a glow discharge.

15 In order to achieve the maximum difference in thermal conductivity between adjacent layers 97,98 the interfaces 99 between the adjacent layers 97,98 are kept as abrupt as is practical. The abrupt interfaces 99 are preferably achieved by the use of a simple switching
20 action as shown in region B of figure 11 between the physical vapour deposition process such that the voltage at the substrate follows a square wave form with time. The peak voltage in region B of figure 11 correspond to the time when the layers 97 of ceramic are deposited by
25 PAPVD and the minimum voltages in region B of figure 11 correspond to the time when the layers 98 of ceramic are deposited by PVD. The switching points correspond to the time when the interfaces 99 are produced.

30 The current drawn in the circuit as a function of substrate voltage is shown in figure 12, more current is drawn as the voltage increases. In order to sustain a glow discharge for the plasma assisted physical vapour deposition process, in this configuration for electron beam evaporation, the minimum voltages are of the order
35 of three hundred volts as shown in figure 13, and the current densities are typically greater than 0.1 mA/sq cm. This increases at any given pressure with applied

substrate voltage.

In another experiment the structurally modulated thermal barrier coating was produced by switching between a DC applied substrate bias, having a peak voltage of 5 2000 volts (negative), and ground. The time interval was 1 minute at each of the voltage levels and the pressure was 10 mtorr. Figure 14 is a scanning electron micrograph of a fracture cross-section through the thermal barrier coating. The continuous columnar grains 10 can be seen extending through the full thickness of the thermal barrier coating and the modulated structure of the columns is evident. The outer portion of the coating 15 was deposited purely in the PVD mode.

The voltage applied to the substrate during the 20 plasma assisted physical vapour depositions part of the process is sufficient to cause densification of the thermal barrier coating but is not sufficient to cause renucleation/grain growth within the structure with subsequent loss of the major, through thickness, columnar boundaries.

The physical vapour deposition process described uses electron beam evaporation, however, other physical vapour deposition processes may be used for example sputtering or arc evaporation.

25 Although the description has referred to physical vapour deposition to deposit the ceramic thermal barrier coating it may be equally possible to deposit the ceramic thermal barrier coating by chemical vapour deposition. The alternate layers may then be deposited using chemical 30 vapour deposition and plasma assisted chemical vapour deposition.

The thermal barrier coatings described in the examples are ceramic materials, however the thermal barrier coating may be any suitable material of low 35 thermal conductivity. Materials suitable for use as thermal barrier coatings are generally oxides, for example zirconia, yttria, hafnia, ceria or combinations

of any two or more thereof.

The different layers in the thermal barrier coating are intended to have substantially the same composition, however the process of applying the thermal barrier

5. coating may result in some compositional differences between the different layers.

There appears to be an optimum spacing between the layers of ceramic for improved thermal conductivity when comparing the results of the third and fourth coating

10 systems to the first coating system.

Claims:-

1. An article (10) comprising a metallic substrate (20), a bond coating (22) on the metallic substrate (20), a thermal barrier coating (24) on the bond coating (22), the thermal barrier coating (24) comprising a plurality 5 of layers (25,27), characterised in that each layer (25,27) has columnar grains (28), the columnar grains (28) in each layer (25,27) extend substantially perpendicular to an interface between the bond coating (22) and the metallic substrate (20), adjacent layers 10 (25,27) have different structures to provide at least one interface (26) between adjacent layers (25,27) which is substantially parallel to the interface between the bond coating (22) and the metallic substrate (20) to increase the resistance to heat transfer through the thermal 15 barrier coating (24).
2. An article as claimed in claim 1 in which the metallic substrate (20) is a superalloy substrate.
3. An article as claimed in claim 2 in which the superalloy substrate (20) is a nickel superalloy 20 substrate.
4. An article as claimed in any of claims 1 to 3 in which the bond coating (22) comprises a MCrAlY coating, an aluminide coating, a platinum aluminide coating or a combination of any two or more thereof.
- 25 5. An article as claimed in claim 4 in which the bond coating (92) includes an interface layer (94) comprising an oxide or oxide/metal, the thermal barrier (96) coating being on the interface layer (94).
6. An article as claimed in any of claims 1 to 5 in 30 which the thermal barrier coating (24) is formed from a ceramic material.
7. An article as claimed in claim 6 in which the ceramic material comprises zirconia, yttria or a mixture thereof.
- 35 8. An article as claimed in any of claims 1 to 7 in which alternate layers (25) of the thermal barrier

coating (24) have substantially the same structure.

9. An article as claimed in claim 8 in which adjacent layers (25,27) have substantially the same thickness.

10. An article as claimed in any of claims 1 to 9 in 5 which the thickness of each layer (25,27) is in the range of 0.5×10^{-6} m to 10×10^{-6} m.

11. An article as claimed in claim 10 in which the thickness of each layer (25,27) is 2×10^{-6} m.

12. An article as claimed in any of claims 1 to 11 in 10 which the total thickness of the thermal barrier coating (24) is equal to or less than 300×10^{-6} m.

13. An article as claimed in any of claims 1 to 12 in which the layer adjacent the bond coating (22) has a high density.

15 14. An article as claimed in claim 13 in which the layer adjacent the bond coating (22) has maximum density.

15. An article as claimed in any of claims 1 to 14 in which the article (10) is a turbine blade or turbine vane.

20 16. A method of manufacturing an article (10) comprising applying a bond coating (22) to a metallic substrate (20), applying a thermal barrier coating (24) to the bond coating (22) by depositing at least one columnar grained layer (27) by vapour deposition and depositing at least 25 one columnar grained layer (25) by plasma assisted vapour deposition to provide an interface (26) between the adjacent layers (25,27) which is substantially parallel to the interface between the bond coating (22) and the metallic substrate (20) to increase the resistance to 30 heat transfer through the thermal barrier coating (24).

17. A method as claimed in claim 16 comprising depositing the columnar grained layers (27) by vapour deposition alternately with the columnar grained layers (25) deposited by plasma assisted vapour deposition.

35 18. A method as claimed in claim 16 or claim 17 comprising depositing the columnar grained layer (25) adjacent to the bond coating (22) by plasma assisted

vapour deposition such that it has a high density.

19. A method as claimed in claim 18 comprising depositing the columnar grained layer (25) adjacent to the bond coating (22) such that it has maximum density.

5 20. A method as claimed in any of claims 16 to 19 comprising applying an electrical bias to the metallic substrate (90) and supplying oxygen to modify the bond coating (92) surface to produce an interface layer (94) comprising oxide or oxide/metal prior to deposition of

10 the columnar grained layers (97,98) by the vapour deposition process.

21. A method as claimed in claim 20 comprising applying an electrical bias to the metallic substrate (90) and supplying an inert gas to produce ions to clean the

15 surface of the bond coating (92) prior to the formation of the interface layer (94).

22. A method as claimed in any of claims 16 to 23 comprising depositing the columnar grained layers (27) deposited by vapour deposition and the columnar grained

20 layers (25) deposited by plasma assisted vapour deposition such that they have substantially the same thickness.

23. A method as claimed in any of claims 16 to 23 in which the vapour deposition process is physical vapour

25 deposition.

24. A method as claimed in claim 23 in which the physical vapour deposition process is electron beam evaporation, sputtering or arc evaporation.

25. A method as claimed in any of claims 16 to 24

30 comprising depositing the columnar grained layers (25,27) to a thickness in the range of 0.5×10^{-6} m to 10×10^{-6} m.

29. A method as claimed in any of claims 16 to 25 comprising depositing the columnar grained layers (25,27) to a total thickness equal to or less than 300×10^{-6} m.

35 27. A method as claimed in claim 25 in which the thickness of the columnar grained layers (25,27) is 2×10^{-6} m.

28. A method as claimed in any of claims 16 to 27 comprising applying the bond coating (22) by thermal spraying.

29. A method as claimed in any of claims 16 to 28 in 5 which the bond coating (22) comprises a MCrAlY coating, an aluminide coating, a platinum aluminide coating or a combination of any two or more thereof.

30. A method as claimed in any of claims 16 to 29 in 10 which the metallic substrate (20) is a superalloy substrate.

31. A method as claimed in any of claims 16 to 30 in which the thermal barrier coating (24) comprises a ceramic material.

32. A method as claimed in claim 31 in which the ceramic 15 material is zirconia, yttria or a mixture thereof.

33. An article (10) comprising a metallic substrate (20), a bond coating (22) on the metallic substrate (20), a thermal barrier coating (24) on the bond coating (22), the thermal barrier coating (24) having columnar grains 20 (28), the columnar grains (28) extending substantially perpendicular to an interface between the bond coating (22) and the metallic substrate (20), characterised in that each of the columnar grains (28) in the thermal barrier coating (24) comprises a plurality of layers 25 (25,27), adjacent layers (25,27) have different structures to provide at least one interface (26) between adjacent layers (25,27) which is substantially parallel to the interface between the bond coating (22) and the metallic substrate (20) to increase the resistance to 30 heat transfer through the thermal barrier coating (24).

34. A method of manufacturing an article (10) comprising applying a bond coating (22) to a metallic substrate (20), applying a thermal barrier coating (24) to the bond coating (22) by applying a first voltage to the metallic 35 substrate (20) and depositing at least one columnar grained layer (27) by vapour deposition, substantially instantaneously applying a second different voltage to

the metallic substrate (20) and depositing at least one columnar grained layer (25) by vapour deposition to provide an interface (26) between the adjacent layers (25, 27) which is substantially parallel to the interface 5 between the bond coating (22) and the metallic substrate (20) to increase the resistance to heat transfer through the thermal barrier coating (24).

35. A method as claimed in claim 34 in which the first voltage applied is zero volts.

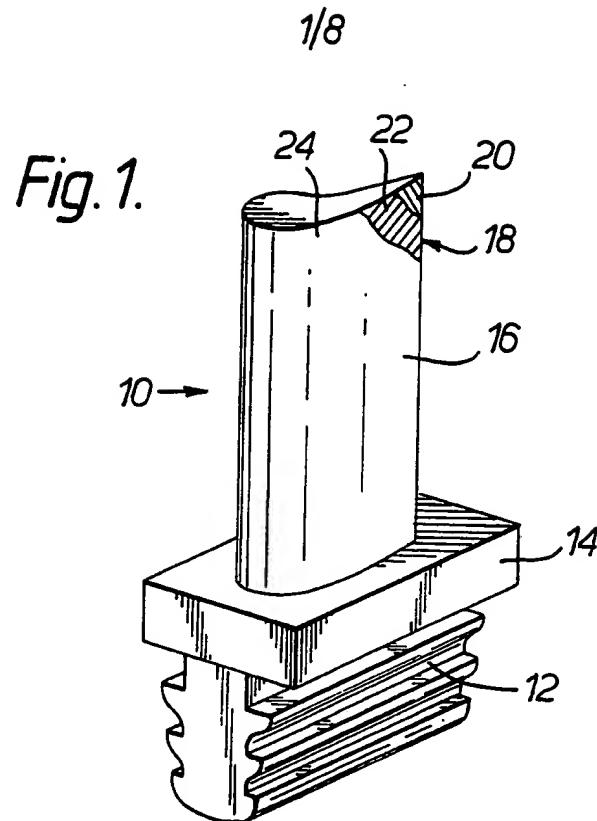
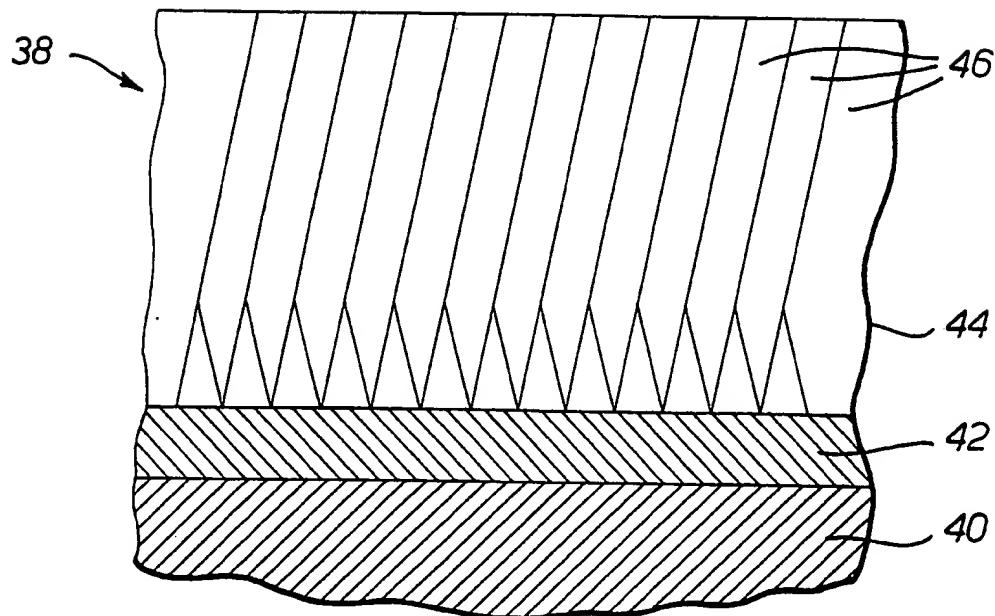


Fig. 2.



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Fig. 3.

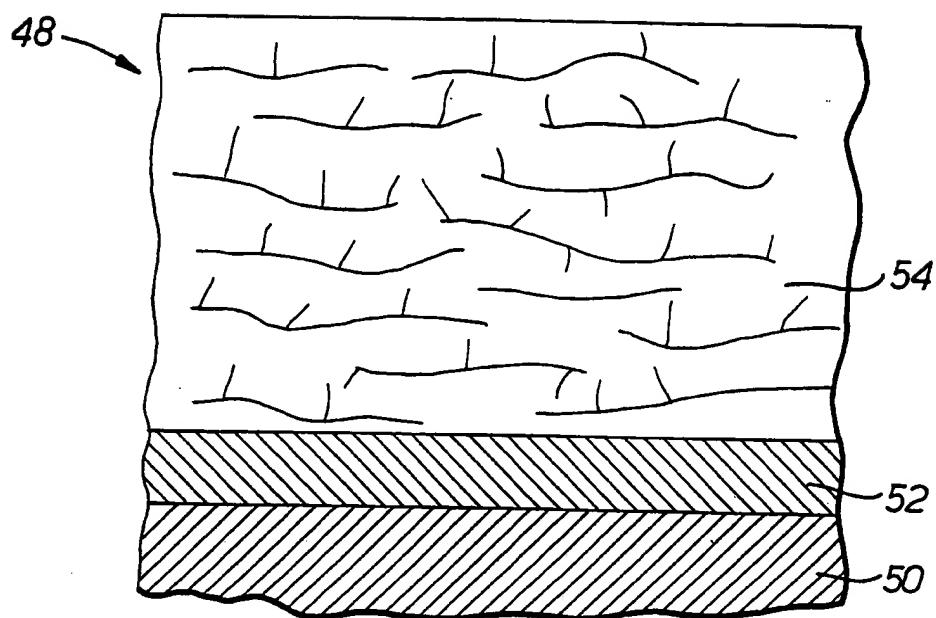
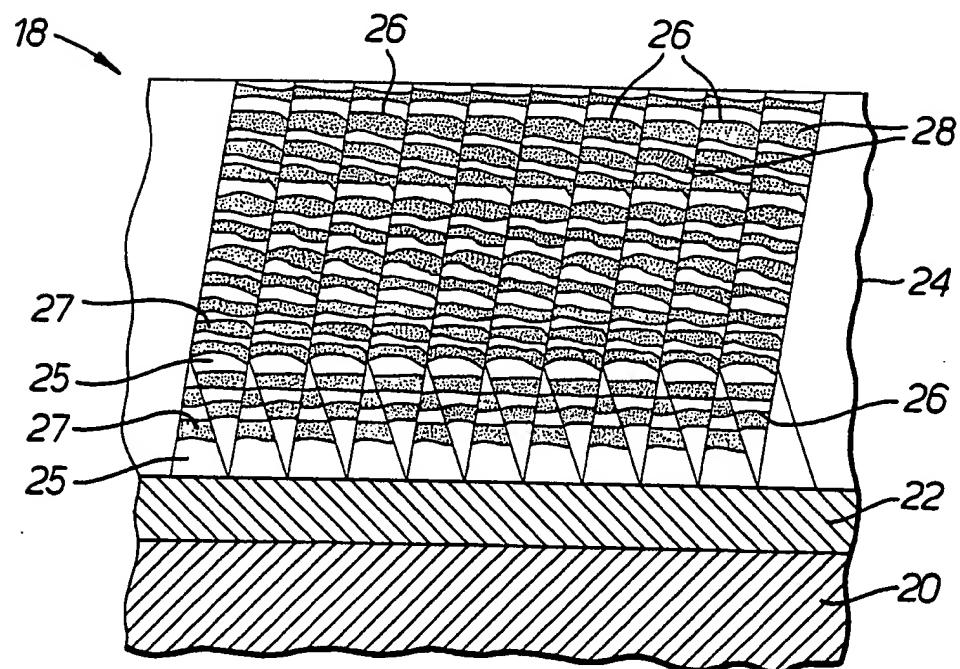


Fig. 4.



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Fig.5.

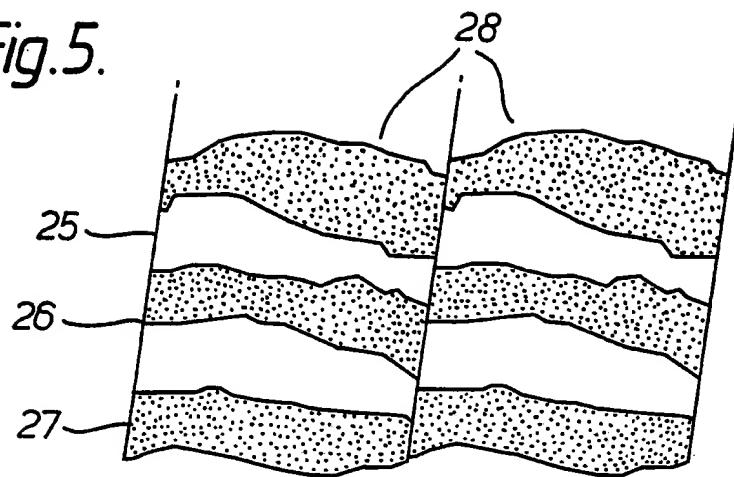
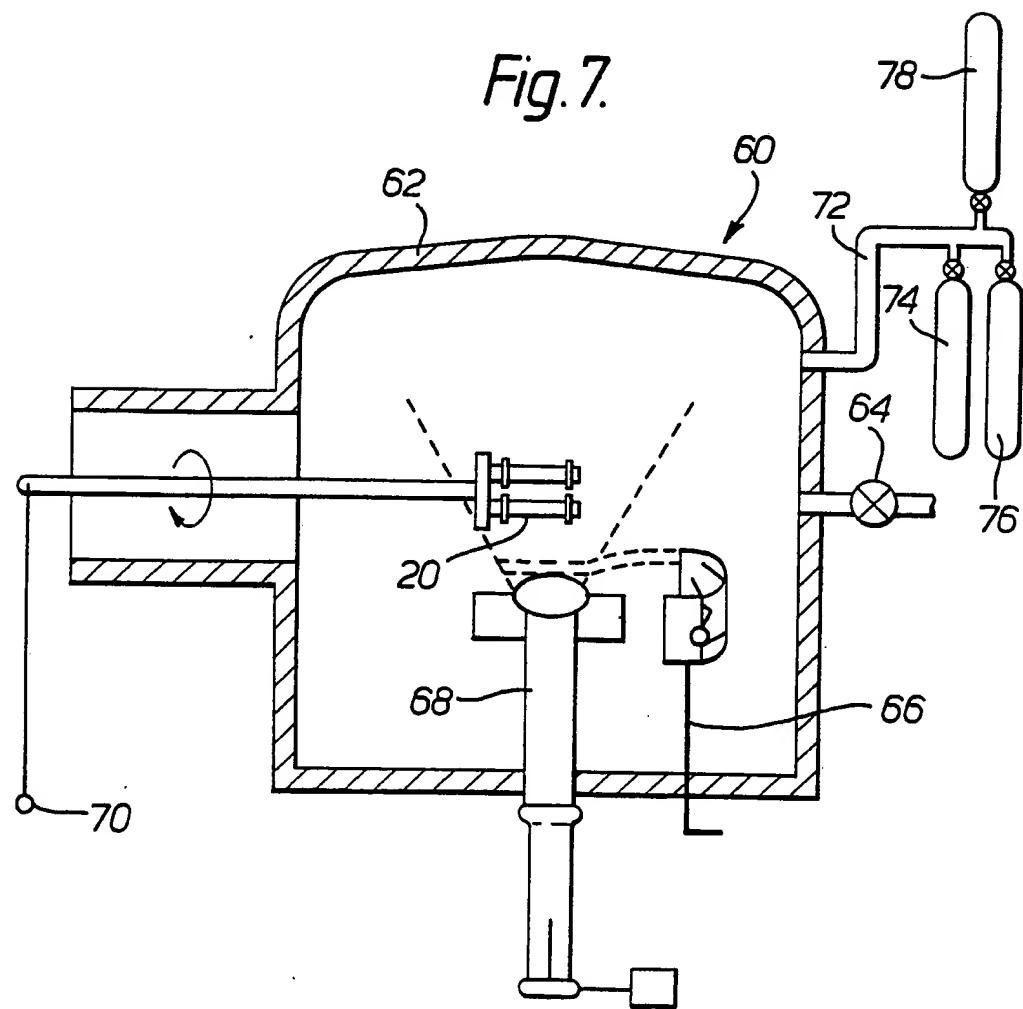


Fig.7.



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Fig. 6.

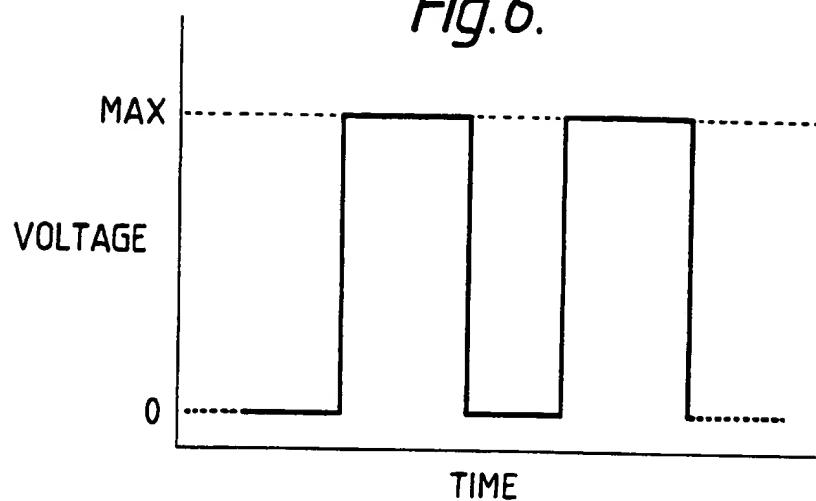
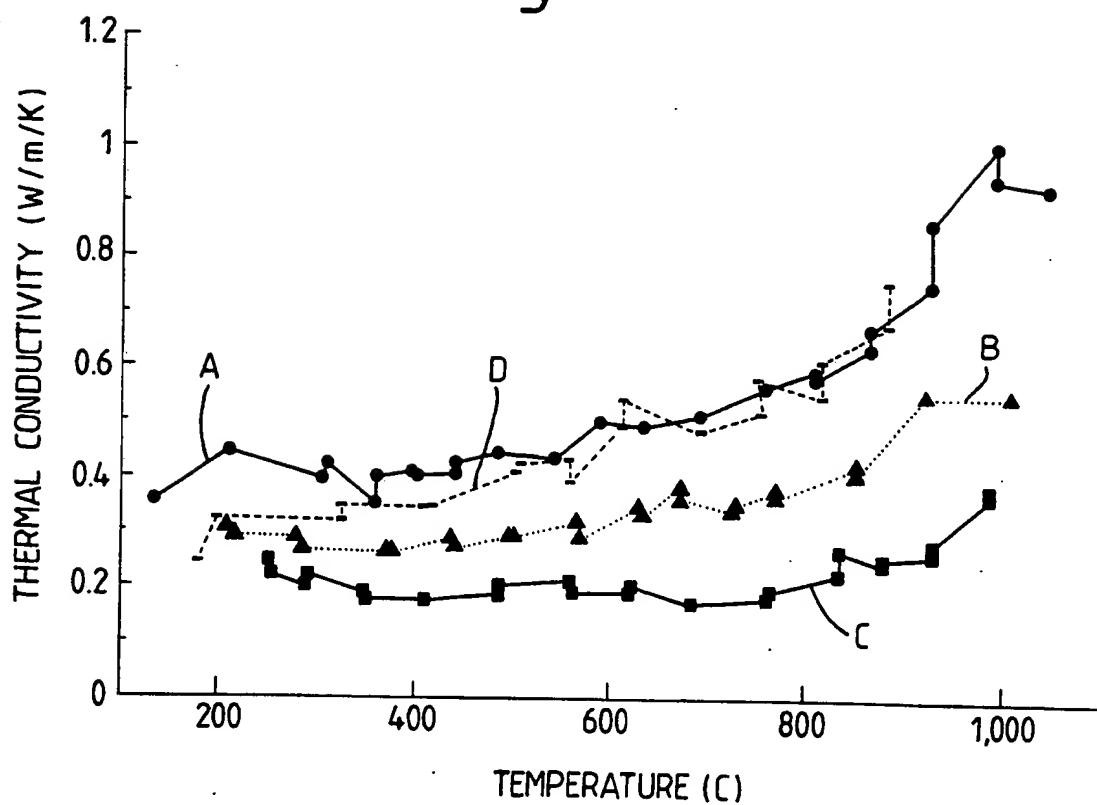


Fig. 8.



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Fig. 9.

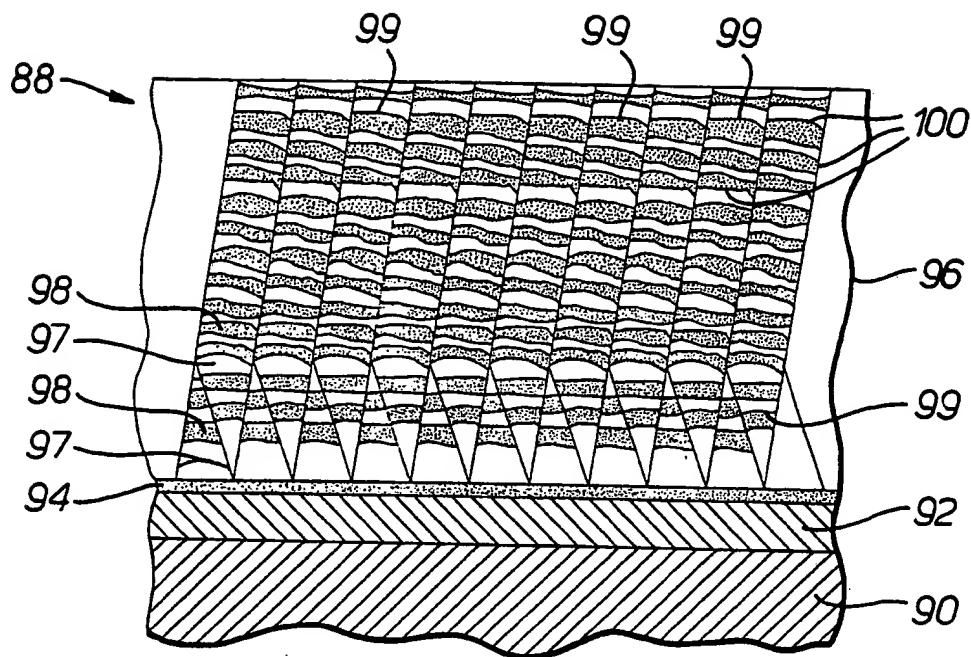
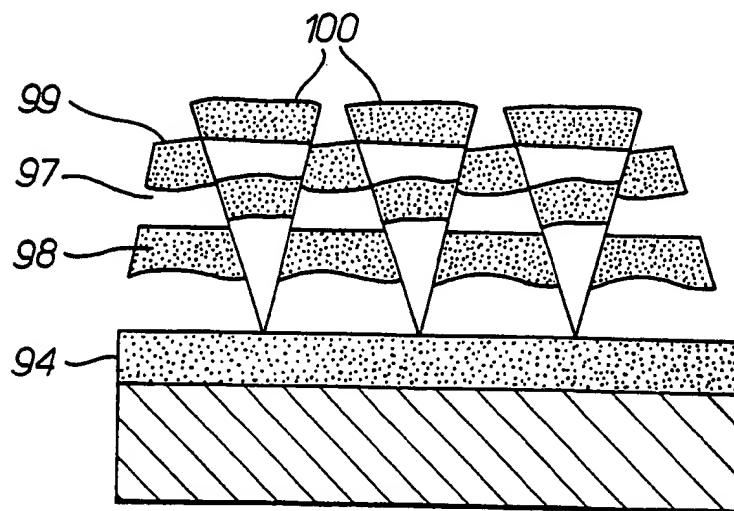


Fig. 10.

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Fig.11.

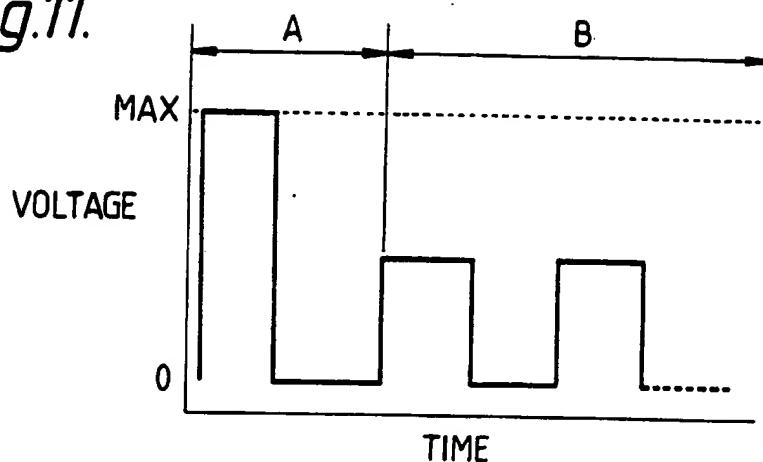
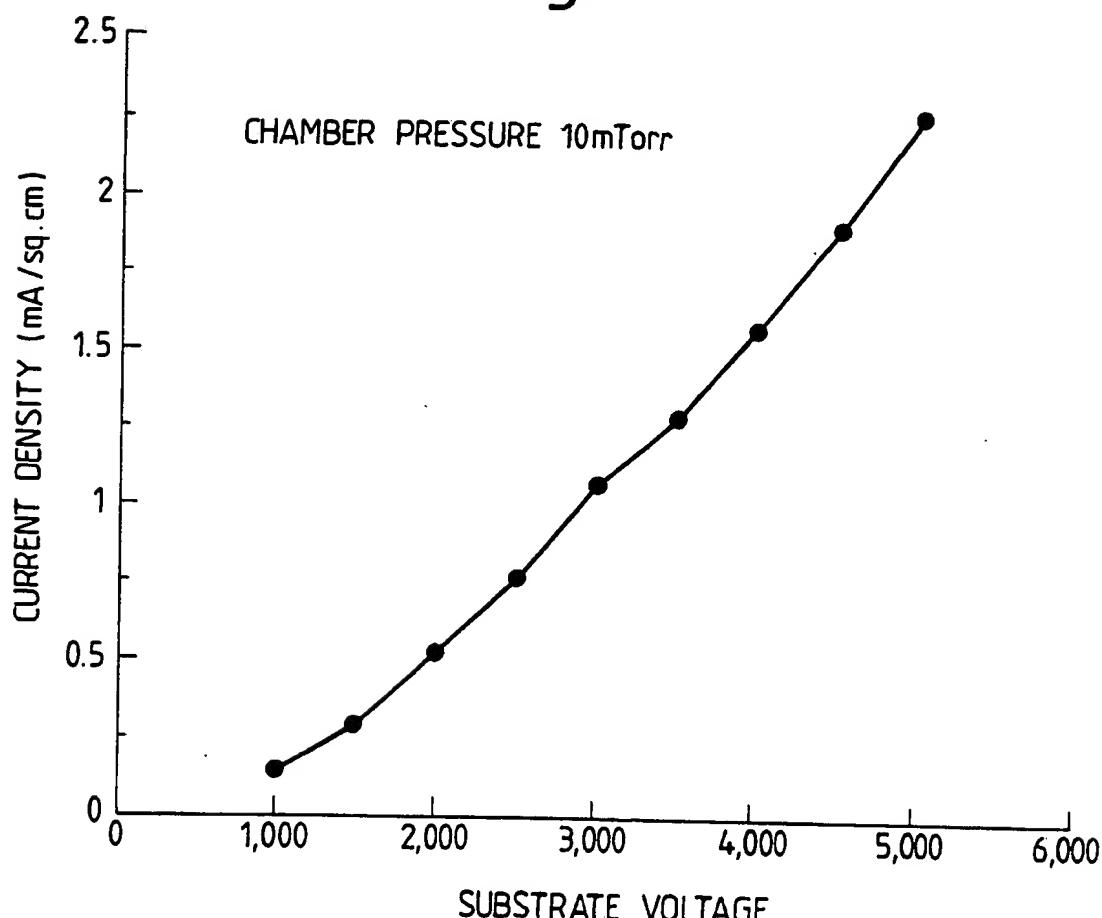


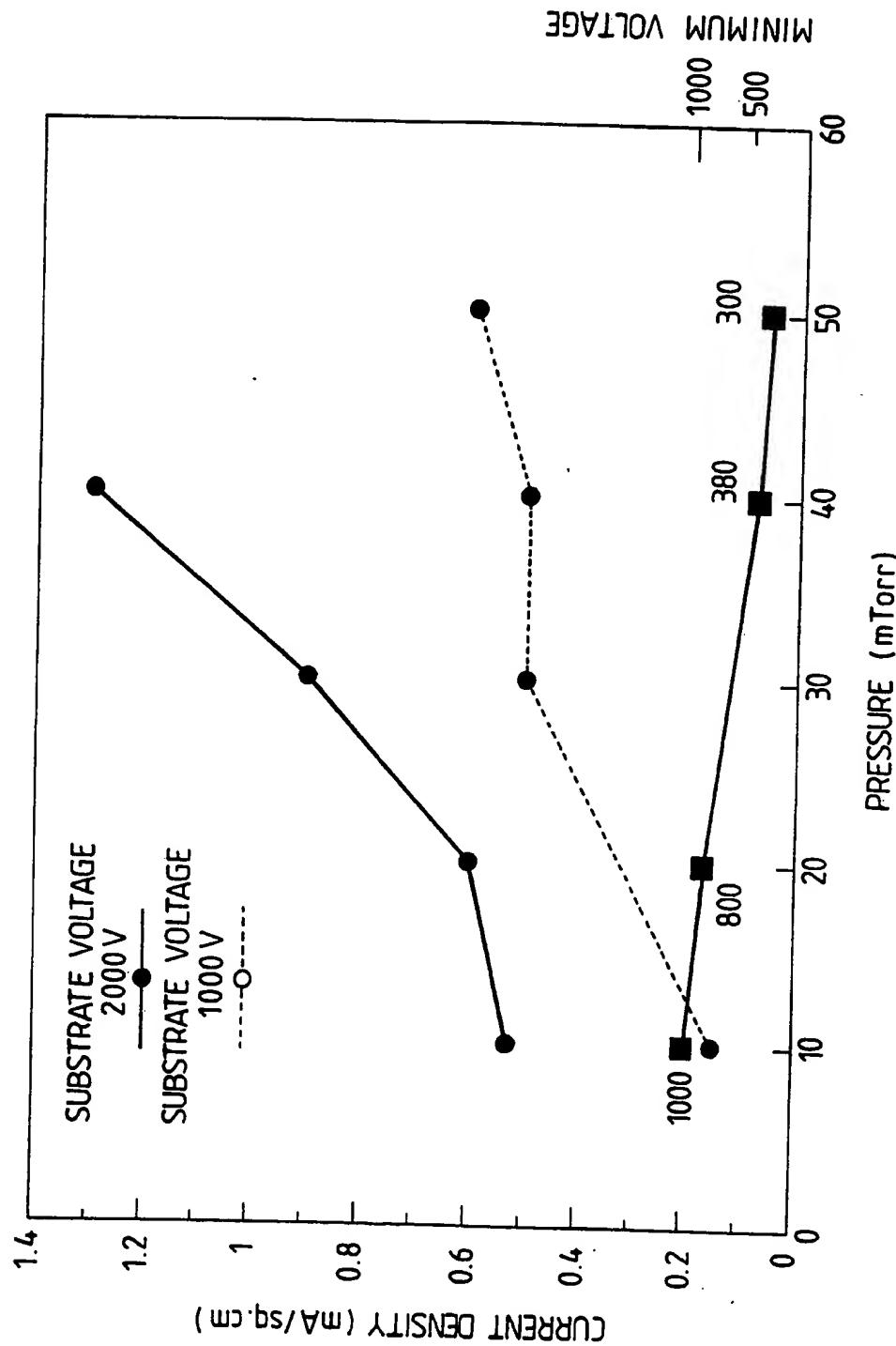
Fig.12.



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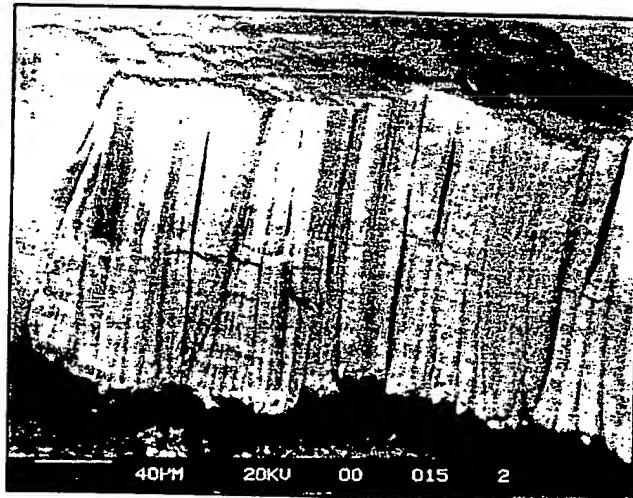
Fig.13.



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Fig.14.



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INTERNATIONAL SEARCH REPORT

International Application No.

PCT/GB 93/00441

I. CLASSIFICATION OF SUBJECT MATTER (If several classification symbols apply, indicate all)⁶

According to International Patent Classification (IPC) or to both National Classification and IPC

Int.C1. 5 C23C14/08; C23C28/00; F01D5/00

II. FIELDS SEARCHED

Minimum Documentation Searched⁷

Classification System	Classification Symbols
Int.C1. 5	C23C ; F01D

Documentation Searched other than Minimum Documentation
to the Extent that such Documents are Included in the Fields Searched⁸III. DOCUMENTS CONSIDERED TO BE RELEVANT⁹

Category ¹⁰	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²	Relevant to Claim No. ¹³
A	<p>SURFACE AND COATINGS TECHNOLOGY vol. 32, 23 March 1987, LAUSANNE CH pages 389 - 397</p> <p>J.T. PRATER ET AL 'CERAMIC THERMAL BARRIER COATINGS WITH IMPROVED CORROSION RESISTANCE' cited in the application see page 391, line 12 - line 31</p> <p>-----</p> <p>THIN SOLID FILMS vol. 127, no. 1/2, May 1985, LAUSANNE CH pages 93 - 105</p> <p>T.E. STRANGMAN 'THERMAL BARRIER COATINGS FOR TURBINE AIRFOILS' see page 100, line 29 - page 101, line 3</p> <p>-----</p> <p>US,A,4 916 022 (P.A.SOLFEST ET AL) 10 April 1990 see column 5, line 62 - column 6, line 36</p> <p>-----</p>	1-35
A		1-35
A		1-35

¹⁰ Special categories of cited documents:

- ^A document defining the general state of the art which is not considered to be of particular relevance
- ^E earlier document but published on or after the international filing date
- ^L document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- ^O document referring to an oral disclosure, use, exhibition or other means
- ^P document published prior to the international filing date but later than the priority date claimed

^T later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention^X document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step^Y document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.^Z document member of the same patent family

IV. CERTIFICATION

Date of the Actual Completion of the International Search

04 JUNE 1993

Date of Mailing of this International Search Report

23.06.93

International Searching Authority

EUROPEAN PATENT OFFICE

Signature of Authorized Officer

EKHULT H.U.

III. DOCUMENTS CONSIDERED TO BE RELEVANT (CONTINUED FROM THE SECOND SHEET)

Category °	Citation of Document, with indication, where appropriate, of the relevant passages	Relevant to Claim No.
A	<p>EP,A,0 366 924 (ALLIED-SIGNAL INC) 9 May 1990 see example 1</p> <p>-----</p>	1-35

ANNEX TO THE INTERNATIONAL SEARCH REPORT
ON INTERNATIONAL PATENT APPLICATION NO.

GB 9300441
SA 71221

This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on The European Patent Office is in no way liable for those particulars which are merely given for the purpose of information. 04/06/93

Patent document cited in search report	Publication date	Patent family member(s)		Publication date
US-A-4916022	10-04-90	None		
EP-A-0366924	09-05-90	US-A- 4880614 US-A- 5015502		14-11-89 14-05-91